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# Nanoporous Pt-based catalysts prepared by chemical dealloying of magnetron-sputtered Pt-Cu thin films for the catalytic combustion of hydrogen



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#### ABSTRACT

In this work, we prepared SiC-supported Pt-Cu thin films by magnetron sputtering for use as catalysts for the combustion of hydrogen under oxidizing conditions. We tested the catalysts as prepared and after chemical dealloying. A methodology is presented to fabricate catalytic thin films of a desired composition with tailored magnetron targets with lower Pt consumption. The deposition gas was changed to prepare columnar (Ar-deposited) and closed-porous (He-deposited) films to study the effect of the microstructure on the activity. The effect of composition was also studied for the columnar samples. The as-prepared Pt-Cu thin films showed significant activity only at temperatures higher than  $100\,^{\circ}\text{C}$ . Dealloying permitted an increase in the activity to achieve near room-temperature activity. The dealloyed closed-porous He-deposited sample was the most active, being able to convert as much as  $13.15\,\,\text{L}_{\text{H2}}\text{min}^{-1}\,\,\text{g}_{\text{Pt}}^{-1}$  at  $70\,^{\circ}\text{C}\,\,(\text{E}_{\text{a}} = 1\,\,\text{kJ}\,\,\text{mol}^{-1})$ . This sample was preferentially dealloyed on the surface, yielding an almost pure Pt shell (96% at. Pt) and a Cu-depleted interior (71% at. Pt). This compositional inhomogeneity enabled the sample to achieve enhanced activity compared to the Ar-deposited columnar sample (with similar initial composition, but uniformly dealloyed), probably due to the compressive surface lattice strain. The dealloyed closed-porous He-deposited sample was shown to be durable over five cycles.

## 1. Introduction

The catalytic combustion of hydrogen (CHC, reaction 1) is a highly exothermic reaction ( $-286\,\mathrm{kJ\,mol}^{-1}$ ) that is very interesting from both a fundamental and an applied point of view. Due to its relative simplicity it can be considered as model catalytic oxidation reaction in the gas phase, and has applications in heaters for domestic or industrial use (for example, cooking, heating spaces, floors and walls, drying and other heating industrial processes) or in safety devices [1–5].

$$H_2(g) + 1/2 O_2(g) \rightarrow H_2O(g)$$
 (1)

Regarding safety applications, the CHC can be employed as a controllable means to eliminate the undesired amounts of hydrogen in installations such as in the nuclear industry or fuel cell-based power generation devices [3–8]. The elimination of residual hydrogen from the exhaust gases from fuel cells requires the use of catalysts that are active at room temperature (RT). According to previous studies, only Pt and Pd can catalyse the reaction at low temperatures [1]. However,

these are scarce and precious metals, increasing the costs of any possible application. For this reason, the development of highly active and stable Pt or Pd-based catalysts with low precious metal content by cost-effective methods is of utmost interest currently.

Many efforts have been made to achieve this goal. The reduction in metal loading in Pt-impregnated catalysts, alloying with other less expensive metals such as Ni, Cu and Co, the use of reducible supports such as  $CeO_2$  and ionic Pt or Pd substitution on oxidic supports, are the most employed methods in the literature [4,5,9–11].

Another strategy to obtain highly active noble metal catalysts for CHC is dealloying. Dealloying is an ancient practice based on the selective dissolution of the less noble component of a bimetallic precursor to obtain a nanoporous (np) material enriched in the nobler component [12–14]. This process can be conducted either electrochemically or chemically reducing the consumption of noble elements by more than 70% [15–20]. Compared to electrochemical dealloying, chemical dealloying is more practical and scalable in the catalyst industry [20] and can also be applied for supported films on non-conductive supports.

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Dealloying has been successfully used to enhance the catalytic activity of Pt-Cu nanoparticles or nanofilms for the oxygen reduction reaction (ORR) [15–23a]. This process leads to the formation of a Cu-depleted interior covered by a Pt surface layer that is compressively strained, resulting in a downshift and broadening of the Pt d-band and leading to a weaker oxygen bond strength and higher ORR activity[19, 22,23a].

To our knowledge, the study of the CHC over dealloyed catalysts has not been reported before. In this work, we have prepared Pt-Cu alloy thin films by magnetron sputtering to investigate the effect of chemical dealloying on the activity for the CHC under conditions that simulate the composition of the exhaust gas of a fuel cell ( $1\% \text{ v/v H}_2$  in air). Dealloyed Pd-Cu materials were reported to be less strained than their Pt-containing counterparts, and for this reason they were excluded from this work, despite the lower cost of Pd with respect to Pt [23b].

Magnetron sputtering, a versatile deposition technique widely used in industry, permits the design of catalytic thin films with controlled microstructure and composition, over a wide variety of supports to obtain model catalysts for structure-performance studies [24–27]. Pt-Cu catalysts fabricated by magnetron sputtering have been previously investigated either by co-sputtering from Cu and Pt targets or by sputtering alloyed targets with the desired composition [22,24]. Their structure before and after dealloying has been correlated with the ORR activity [22].

In this work, we have developed a preparation process that minimizes the Pt consumption. We propose a cost-effective strategy to prepare alloy coatings using a Cu target with Pt strips. The approach is flexible regarding target composition (by adding or removing strips) in contrast to an alloy target of fixed composition. Additionally, over the last years, we have developed in our laboratory a simple methodology for the bottom-up fabrication of closed-porous coatings using helium plasmas [28,29]. The influence of this singular microstructure on the chemical dealloying process and on the CHC activity is investigated here and compared to columnar coatings deposited with Ar of similar composition. We prepared two low Pt-content Pt-Cu samples with similar compositions and different microstructures (i.e., columnar vs. closed porous) by using different sputtering gases (Ar and He respectively). We also prepared a third sample with higher Pt content using Ar as the sputtering gas to study the effect of composition for columnar films. The influence of microstructure and composition on the activity of both the as- prepared and dealloyed thin films will be discussed in this paper.

## 2. Experimental section

## 2.1. Samples preparation

Coatings were deposited by sputtering under pure Ar or He

atmosphere using a 2" magnetron from the Thin Film Consulting Company. A scheme of the deposition geometry is represented in Fig. 1a. Pt-Cu targets were prepared from a pure copper target (Kurt J. Lesker, 99.99% pure, 5 mm thick) on which Pt strips (Goodfellow, 99.99% pure, 0.15 mm thick) were radially distributed as shown schematically in Fig. 1b. Two Pt-Cu targets were prepared by varying the number of the Pt strips (see Table 1). A pure copper target was also used to prepare pure Cu reference coatings. The base pressure before deposition was  $10^{-6}$  mbar while the working pressure was  $4.8 \times 10^{-2}$ mbar (for either Ar or He, 99.9995% purity). The deposition power was 100 W in RF mode. The substrates to be coated were placed on a rotary sample-holder to ensure homogeneous deposition. The cathode was placed parallel to the substrates at a distance of 5 cm from the sampleholder (Fig. 1a). Table 1 summarizes the deposition conditions employed as well as deposition times, deposition rates and thicknesses of the fabricated samples.

The composition of the coatings was determined after adequate digestion by inductively coupled plasma atomic emission spectroscopy (ICP-AES) as described in the subsection "Characterization" in this experimental part. Table 1 also summarizes the abbreviated names used for all of the coatings, which were based on the obtained coating compositions and the process gas used. The precise substrate used will be indicated when necessary.

All of the coatings were deposited in the conditions described above directly onto different substrates: i) PTFE (polytetrafluoroethylene) membranes (Pall Corporation,  $0.02\,\mu m$  pore size, polypropylene backed), used as received, for characterization. ii) A commercial alumina bonded SiC monolith foam (VUKOPOR\*S100 from LANIK with 100 pores per inch (ppi)) for the catalytic studies of the CHC reaction and the characterization [8]. These substrates were washed in an ultrasonic bath successively with distilled water and ethanol/acetone (1:1) and then dried in vacuum at  $110\,^{\circ}\text{C}$  overnight. iii) Si (100) pieces cleaned with acetone and dried in a nitrogen flow, for characterization.

Dealloyed samples (d-samples) were obtained by treating the films under concentrated nitric acid (14.4 M) for 5 min at room temperature. After dealloying, the samples were washed thoroughly with deionized water until neutral pH and dried in a vacuum oven at  $110\,^{\circ}$ C.

#### 2.2. Characterization

Scanning Electron Microscopy (SEM) analyses were performed on silicon and SiC foam-supported films in a high-resolution SEM-FEG (Field Emission Gun) microscope (Hitachi S4800) operated at 5 keV for imaging and at 20 keV for compositional analysis. The microscope is equipped with a Bruker X-Flash 4010 EDX (Energy Dispersive X-ray) detector.

X-ray diffraction (XRD) measurements on the Si-supported films

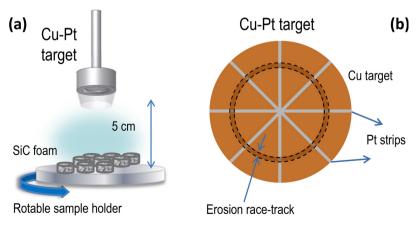


Fig. 1. Schemes representing (a) the MS deposition geometry and (b) the Pt strips distribution on the Cu target (the erosion race-track is indicated by the dotted rings).

**Table 1**Deposition conditions and bulk composition of the as-prepared Cu and Pt-Cu thin films.

Sample name	Target	Pt/Cu area ratio at the race- track <sup>a</sup>	dep. gas	dep. time (min)	Thickness (nm)	dep. Rate (nm/min)	at.% Pt (ICP)	at. % Cu (ICP)
Cu_He	Cu	0	Не	24	250	10	_	_
Cu_Ar	Cu	0	Ar	8	400	50	_	_
Low Pt-Cu_He	PtCu	0.43	He	37.5	300	8	13	87
Low Pt-Cu_Ar	PtCu	0.12	Ar	7.5	370	49	13	87
High Pt-Cu_Ar	PtCu	0.43	Ar	7.5	400	53	41	59

a Pt/Cu area ratio at the target erosion race-track controlled by the number and width of the Pt strips on a Cu target.

were performed using Cu K $\alpha$  radiation in a Siemens D5000 diffractometer in a Bragg-Brentano configuration in the 2 $\theta$  angle range of 10–90°. Crystallite size was calculated using the X-Pert High Score Plus software with a 0.9 value for Scherrer's constant.

X-ray photoelectron spectroscopy (XPS) spectra of the PTFE-supported films were recorded with a SPECS electron spectrometer, equipped with a PHOIBOS 150 hemispherical analyser, using Al Ka radiation with a 35 eV pass energy at the normal emission take-off angle. The spectra were calibrated with the signal of C 1s at 284.6 eV from adventitious carbon.

For TEM (transmission electron microscopy) studies, SiC-supported dealloyed Pt-Cu films were ground in a mortar to obtain a powder. Measurements were performed employing a Philips CM20 microscope (operated at 200 kV) and an FEI Tecnai G2 F30 FEG (field emission gun) microscope (operated at 300 kV).

Samples deposited on PTFE were submitted to digestion before being analysed by ICP-AES (inductively coupled plasma atomic emission spectroscopy) at the CITIUS laboratories (University of Seville) to quantify the Pt and Cu atomic percentages.

#### 2.3. Catalytic tests

The catalytic combustion of hydrogen was tested under oxidizing conditions for the monolithic SiC-supported thin film catalysts in a quartz reactor (20 mm diameter, 500 mm length). The film thickness (300 nm) was optimized to achieve a sigmoid conversion vs. temperature curve. These conditions are essential to evaluate and compare catalytic properties (activation energy, T<sub>50</sub>, etc.) in a kinetic regime. Under these conditions, the heat released by the reaction is negligible. Unless indicated otherwise, prior to each test, one SiC monolithic piece coated with a 300 nm catalyst film was loaded onto the reactor. Then, the reactor was fed with 200 mL min<sup>-1</sup> of 1% v/v mixture of H<sub>2</sub> in air. The reactor was heated to 420 °C from the outside using a Hobersal TRO electric furnace and was kept under this temperature for 30 min. After that, the heating was interrupted and the conversion was measured as a function of the temperature in cooling mode. Temperature was measured by a K-type thermocouple placed at the centre of the packed bed. The H<sub>2</sub> content in the outlet of the reactor was measured by an HP 5890 chromatograph equipped with a ShinCarbon ® packed column and a TCD (thermal conductivity) detector with N2 as the carrier gas.

#### 3. Results and discussion

#### 3.1. Microstructure and composition of the as deposited samples

The composition control of the as deposited Pt-Cu thin films with minimized Pt consumption was achieved as follows. The planar magnetron cathode operating in unbalanced configuration leads to a sputter-erosion path with the shape of a closed ring on the flat target denoted as the race-track (see Fig. 1b). In a first approximation we can expect to obtain in the deposited film a Pt/Cu atomic ratio proportional to the area covered in the race-track by Pt vs. Cu with a correction factor given by the different sputtering yields of both elements under each particular deposition condition. The sputtering yields can be estimated from an on-line tool from the TU Wien (https://www.iap.

tuwien.ac.at/www/surface/sputteryield), showing a smaller sputtering yield for Pt than for Cu for the case of helium compared to argon. On this basis, two targets of high (more strips) or low (less strips) Pt content were prepared with the Pt/Cu area ratios at the race-track summarized in Table 1. The obtained compositions of the Pt-Cu samples determined by ICP-AES reflect the values expected from the considerations above, within the experimental error. This demonstrates that our approach is adequate to obtain films at a desired composition without the use of more expensive pure Pt or Pt-Cu targets. Furthermore, the Pt strips are easier to clean and can be recycled and/or reused after each deposition. Regarding the Ar-sputtered films, the atomic Pt-content is 13 and 41% for the low and high Pt content samples (named Low Pt-Cu\_Ar and High Pt-Cu\_Ar, respectively). The thin film prepared using He also has a low Pt content of 13 at. % of Pt, and is named Low Pt-Cu He.

The choice of Ar or He as the process gas influences not only the sputtering yield, and therefore the composition, but also the microstructure of the as-deposited films. Fig. 2 compares SEM micrographs of the as-prepared catalysts using Ar and He as sputtering gases. The two catalysts obtained using Ar (high and low Pt content) show a columnar structure typical for magnetron-sputtered coatings grown under low adatom mobility conditions where surface shadowing governs the film growth [30]. The cross-section images reveal that these meso-columns are composed by nanocolumns where intra and inter-columnar porosity can be observed. On the other hand, the catalyst prepared using He as the sputtering gas exhibits a different microstructure. Closed porosity is clearly visible and homogeneously distributed all along the film thickness (Fig. 2 left) as expected from our previous works, where a new bottom-up methodology was described to grow layers with closed pores nanostructure by magnetron sputtering [28,29,31]. Similar microstructures (see Fig. S1 in Supporting information SI) can be observed for the pure Cu reference samples fabricated in He (porous) and Ar (columnar). EDX measurements, were performed at 20 kV from top-views to estimate the Pt and Cu relation in bulk and the results are shown in Table 2. The values were obtained as an average of the composition measured in several representative zones. The bulk composition obtained by SEM/EDX is in agreement with the results obtained by ICP-AES, within the experimental error. Illustrative elemental map images for the Low Pt-Cu\_He sample deposited on the SiC foam are also included in Fig. S2 (Supporting information). The homogeneous distribution of Pt and Cu indicates the alloy formation, and the quality of the deposition methodology for the fabrication of alloyed catalysts.

XRD measurements were performed and the results are shown in Fig. 3. The three Pt-Cu as deposited catalysts show profiles characteristics of the fcc crystal structure as well as the two reference Cu samples. The Pt-Cu (111) reflections are lying between those of pure Pt (111) and pure Cu (111). Calculation of the crystallite size using the Scherrer's equation (Table 2) shows that samples deposited using Ar as the sputtering gas (Low Pt-Cu\_Ar and High Pt-Cu\_Ar) have a similar crystallite size (approximately 20–21 nm). On the other hand, the sample deposited using He (Low Pt-Cu\_He) has a smaller crystallite size (7 nm) associated with its closed nanoporous structure.

XPS measurements were performed and the normalized spectra are shown in Fig. 4. The study of Pt 4f level, in particular  $4f_{7/2}$ , shows that the platinum in the as deposited samples is essentially metallic Pt $^{\circ}$ 

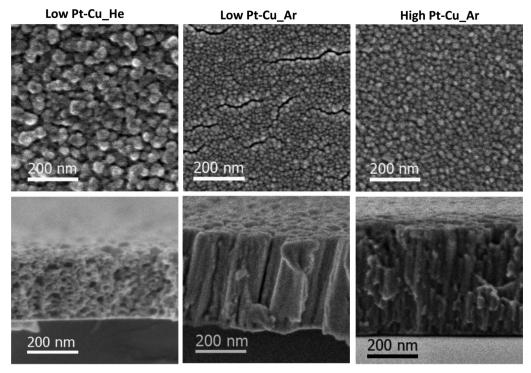


Fig. 2. SEM images (planar view at top, cross section at bottom) of the as-prepared Pt-Cu thin films on Si substrates.

(70–71 eV) with variable contributions of Pt<sup>II</sup> (72 eV) and Pt<sup>IV</sup> (74 eV) states [32]. The position of Pt° for the Low Pt-Cu He/Ar samples is approximately 70.9-71 eV, while for the High Pt-Cu Ar sample is 71.4 eV. The study of Cu 2p level shows the existence of Cu°, Cu<sup>I</sup> and Cu<sup>II</sup> in the three samples. According to the literature, the positions of 2p<sub>3/2</sub> of Cu° and Cu<sup>I</sup> are in the range of 932.6-932.8 eV for pure Cu materials [33]. The presence of  $Cu^{II}$  (2p<sub>3/2</sub>, 933.6 eV) is well identified by the strong satellite peak at + 9 eV from the  $2p_{3/2}$  signal [33]. However, it is known that the position of the Cu 2p level is modified upon alloying. Many papers have reported the shift of Cu° and Cu<sup>I</sup> 2p<sub>3/2</sub> levels to lower binding energies, ranging from 931 eV for Ru-Cu to 931.9 eV for Pt-Cu samples because of the formation of alloys [34–37]. In our samples, the Cu  $2p_{2/3}$  position ranges from 931.0 eV for the High Pt-Cu\_Ar to 931.2 eV for the Low Pt-Cu\_He/Ar samples. This shift to lower binding energies is in accordance with the electron transfer from Pt to Cu upon alloying and is also reflected in the shift to higher binding energies of the Pt 4f<sub>7/2</sub> positions. A similar effect was also reported for Pt alloys with Ni or Fe [38,39].

Quantification of the XPS spectra allowed for the evaluation of the surface composition (Table 2). All coatings exhibit high amounts of surface oxygen, in the 50–60% range for the low Pt content samples (Low Pt-Cu\_He/Ar) and 35% for the High Pt-Cu\_Ar material. This can be correlated to the amount of Pt in the samples. Calculation of the Pt-Cu atomic ratio in the three samples was performed and the results are also summarized in Table 2. From the comparison of the surface Pt-Cu

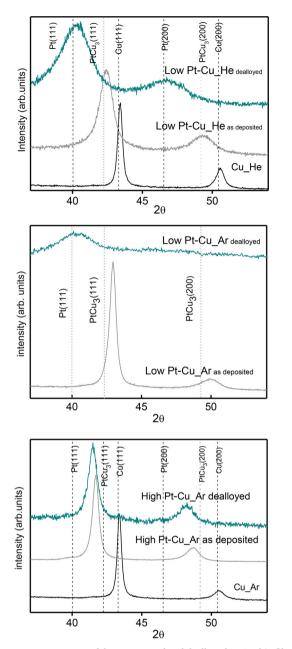
composition with the bulk composition (EDX and ICP), it is possible to conclude that there is a Pt surface segregation effect in the three samples. The Low Pt-Cu\_He sample shows the strongest Pt-segregation, followed by the Low Pt-Cu\_Ar sample. The degree of Pt segregation in the High Pt-Cu\_Ar film is the lowest of the three. This effect can also be interpreted as a result of the lower detectability of the non-noble metal (Cu) at the surface due to its preferential bonding to oxygen.

## 3.2. Microstructure and composition of the dealloyed samples

Dealloyed samples (d-samples) were obtained by treating the films under concentrated nitric acid for 5 min as described in the experimental part. Longer dealloying times were tested but they did not produce further compositional changes. After dealloying, the samples were washed thoroughly with deionized water. A comparative SEM characterization before and after dealloying is shown in Fig. 5 for the films deposited on the SiC foam or PTFE membranes. In these porous substrates, the location of a border in the film allowed to visualize the cross section of the catalyst coatings. The microstructure of the dealloyed samples is similar to that of the as-prepared ones. Closed porous and columnar microstructures are to some extent still visible after the dealloying treatment (see the high magnification images at the bottom of Fig. 5). This is consistent with the dealloying process progressing with a diffusive mechanism, thus avoiding the falling apart of the catalytic coating. Indeed, three-dimensional nanoporous bulk or film

Table 2
Microstructural and chemical characterization of the as-prepared and dealloyed Pt-Cu thin films.

Catalyst State		XRD	Surface composition (XPS)			Surface formula (XPS)	Bulk formula (EDX)	Bulk formula (ICP)
		crystal size (Scherrer)	at.%Pt	at.%Cu	at.%O			
Low Pt-Cu_He	as dep.	7 nm	28.3	17.6	54.1	Pt <sub>0.61</sub> Cu <sub>0.39</sub>	Pt <sub>0.19</sub> Cu <sub>0.81</sub>	Pt <sub>0.13</sub> Cu <sub>0.87</sub>
d- Low Pt-Cu_He	dealloyed	4 nm	54.4	2.1	43.5	$Pt_{0.96}Cu_{0.04}$	$Pt_{0.71}Cu_{0.29}$	Pt <sub>0.72</sub> Cu <sub>0.28</sub>
Low Pt-Cu_Ar	as dep.	20 nm	18.3	19.1	62.6	Pt <sub>0.49</sub> Cu <sub>0.51</sub>	$Pt_{0.16}Cu_{0.84}$	Pt <sub>0.13</sub> Cu <sub>0.87</sub>
d- Low Pt-Cu_Ar	dealloyed	3 nm	30.9	0.6	68.5	$Pt_{0.98}Cu_{0.02}$	$Pt_{0.95}Cu_{0.05}$	Pt <sub>0.92</sub> Cu <sub>0.08</sub>
High Pt-Cu_Ar	as dep.	21 nm	50.2	18.7	31.1	Pt <sub>0.72</sub> Cu <sub>0.28</sub>	Pt <sub>0.44</sub> Cu <sub>0.56</sub>	Pt <sub>0.41</sub> Cu <sub>0.59</sub>
d- High Pt-Cu_Ar	dealloyed	11 nm	66.6	4.4	29	$Pt_{0.94}Cu_{0.06}$	$Pt_{0.5}Cu_{0.5}$	$Pt_{0.45}Cu_{0.55}$



**Fig. 3.** XRD measurements of the as-prepared and dealloyed Pt-Cu thin films on Si substrates.

materials are well reported today [14,40,41]. The formation of a high amount of cracks and voids on the d-Low Pt-Cu\_Ar sample is indicative of the high efficiency of the dealloying process along the film.

The bulk composition of the dealloyed samples was measured by SEM/EDX and ICP-AES, and the results are shown in Table 2. Both methods are in accordance within the experimental error. As expected, the overall dealloying process was more efficient for the Cu-rich samples (Low Pt-Cu\_He and Low Pt-Cu\_Ar) compared to High Pt-Cu\_Ar. This can be attributed to the easier dissolution of the alloy with a higher content of the less noble metal [21]. The highest degree of the overall Pt-enrichment was observed for the d-Low Pt-Cu\_Ar sample in accordance to the SEM images. Dealloyed samples were studied by XRD and the results are shown in Fig. 3. The broad diffraction peaks are symmetric, indicating that the obtained structure is uniform. The Pt-Cu (111) reflections shift to the Pt (111) position, in accordance with the Pt-enrichment. Diffraction peaks after dealloying broaden with respect to their as-prepared counterparts, indicating a decrease in the size of

the crystalline domains. The crystallite size was calculated using the Scherrer's equation and the results are shown in Table 2. The d-High Pt-Cu\_Ar sample has the largest crystallite size (21 nm), while for the d-Low Pt-Cu\_He/Ar samples, the size is much smaller (3–4 nm). This correlates well with the efficiency of the dealloying process for the different samples. The amorphous character of the d-Low Pt-Cu\_Ar/He samples (especially the former, which has a single broad diffraction peak) does not permit accurate simulations in order to compare the bulk lattice strain before and after dealloying.

The microstructure of the d-Low Pt-Cu He/Ar samples on SiC (mortar grinded) was also studied by TEM/HRTEM and the representative micrographs are shown in Fig. 6. This sample preparation method is destructive, and only permits to study some features such as crystalline domains and grains resulting from the grinding process. At high magnification, both dealloyed samples exhibit characteristic nanoporous microstructures with nanocrystalline domains (clearly visible in the insets of Fig. 6) [16]. The d-Low Pt-Cu\_He coating shows 1-4 nm size spherical grains, that are interconnected, mirroring the original closed-porous structure. The d-Low Pt-Cu\_Ar sample also shows grains connected to each other with a similar size range (1-4 nm), although in this case they are not strictly spherical but slightly elongated. The open porous-like structure of this sample is clearly appreciated in the images. HRTEM confirms the results obtained by XRD. The study of several representative images has shown that for both samples the crystal size is approximately 1-4 nm in accordance to Scherrer's calculations (only the biggest particles in the 1-4 nm interval contribute to the broad peaks appreciated in the diffractogram). These studies indicate that both d-Low Pt-Cu\_He/Ar samples have similar grain and crystal size, and the only structural difference is attributed to the type of porosity (more closed vs. more open-like).

XPS surface analysis of d-catalysts was carried out in comparison to the as-prepared ones and the results are shown in Fig. 4. The study of the Pt 4f level shows that after dealloying, the positions of the peaks shift to higher binding energies, according to the oxidation to Pt<sup>II</sup> under the action of concentrated nitric acid. The shift is higher for the samples with lower crystallite size (d-Low Pt-Cu\_He/Ar). The Cu 2p level of the d-Low Pt-Cu\_He/Ar samples is noisy and with low intensity, indicating an efficient depletion of surface Cu and thus the formation of a Pt-enriched surface. The extent of oxidation of Pt is higher for the samples with initial lower amount of the more noble component (Low Pt-Cu\_He/ Ar), where dealloying is progressing more efficiently. These samples show negligible amounts of  $Pt^\circ$  and a mixture of  $Pt^{II}$  and  $Pt^{IV}$  oxidation states, also in accordance to the crystallite size. The d-High Pt-Cu\_Ar sample is still essentially metallic, showing a small decrease in the amount of Pt° with a concomitant small increase in the amount of PtII and  $Pt^{IV}$  oxidation states with respect to the as-prepared sample. The position of the Cu 2p level remains almost unchanged upon dealloying. Calculation of the surface composition by XPS (Table 2) shows that after dealloying, the three samples have an almost pure Pt-surface (94-98% Pt<sub>surface</sub>). However, compared to their corresponding bulk composition (EDX and ICP), it is clear that for the d-High Pt-Cu\_Ar sample, the dealloying process was limited to the first surface layers. In contrast, for the d-Low Pt-Cu He/Ar samples, the process occurred also at the bulk, with selective Cu dissolution observed also in the interior region and not only in the near surface. The Low Pt-Cu Ar sample shows a uniform composition after dealloying (98%  $Pt_{surface}$  vs 95–92%  $Pt_{bulk}$ ), while the dealloyed Low Pt-Cu\_He sample exhibits a Pt surface enrichment compared to the bulk (96%  $\text{Pt}_{\text{surface}}$  vs 72%  $\text{Pt}_{\text{bulk}}\text{), indicating}$ a higher efficiency of the process on the surface layers than in the interior region. This inhomogeneous vertical thin film composition leads to a compressively strained Pt surface, with increased activity with respect to those more relaxed, homogeneous thin film compositions [22,23a]. The d-Low Pt-Cu He sample is also demonstrated to be stable against aqua regia at 80 °C, while the corresponding dealloyed Ar sputtered samples dissolve within a few minutes at RT. All of these results point to the idea that for the low Pt content samples the closed-

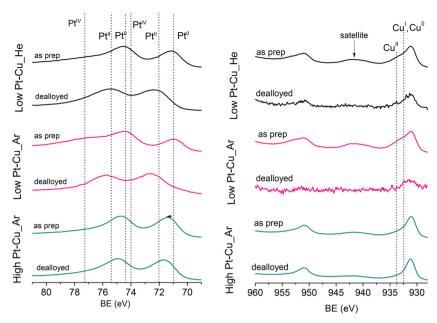


Fig. 4. XPS measurements (normalized spectra) of the as-prepared and dealloyed Pt-Cu thin films on PTFE membrane substrates. Reference binding energy values for the different Pt and Cu oxidation states are indicated.

porous structure presents a higher kinetic barrier to the dealloying process than the columnar one (open porous-like structure).

## 3.3. Catalytic activity of the as deposited samples

Fig. 7 shows the conversion vs. temperature curves for the as-prepared samples in comparison to a pure Cu catalyst (prepared using He

as the sputtering gas) and the reactor itself loaded with bare SiC. As expected, the activity of the Pt-Cu thin films is higher than that of the pure Cu catalyst, but the three samples only show significant activity above 100 °C. The activity in  $L_{\rm H2}\,{\rm min}^{-1}\,{\rm g_{Pt}}^{-1}$  was calculated from the curves at 70 °C and the results (Table 3) indicate that Low Pt-Cu\_He is the most active of the three (2.0  $L_{\rm H2}\,{\rm min}^{-1}\,{\rm g_{Pt}}^{-1}$ ), which correlates inversely with crystal size (Table 2). The activity of both Ar sputtered

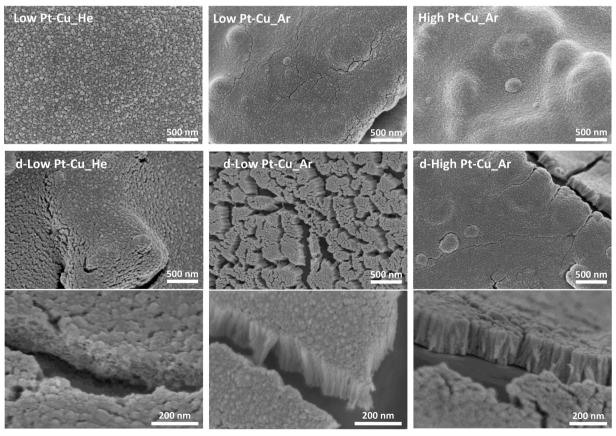


Fig. 5. SEM images of the as-prepared (top row) and dealloyed (rows down) Pt-Cu thin films on SiC or PTFE membrane as substrates.

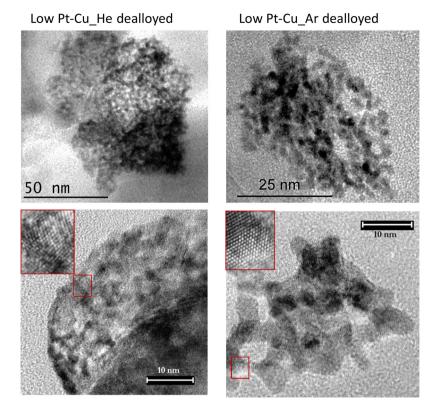


Fig. 6. TEM images of the dealloyed Low Pt-Cu thin films. Insets: zoom of the marked areas.

samples is negligible at that temperature, but a comparison at 50 °C shows that Low Pt-Cu\_Ar is more active (1.95  $L_{\rm H2}\,{\rm min}^{-1}\,{\rm g}_{\rm Pt}^{-1}$ ) than High Pt-Cu\_Ar (negligible activity). For both samples with similar crystal size, the trend can be ascribed to the  $-0.5\,{\rm eV}$  shift in the Pt 4f level of the Low Pt-Cu\_Ar sample with respect to High Pt-Cu\_Ar, according to our previous studies [7].

#### 3.4. Catalytic activity of the dealloyed samples

Fig. 7 shows also the conversion vs. temperature curves for the asprepared samples in comparison to the dealloyed ones. The activity of the dealloyed samples shifts to lower temperatures, achieving near room temperature conversion in all cases. The increase in the activity for all of the dealloyed samples with respect to their as-prepared

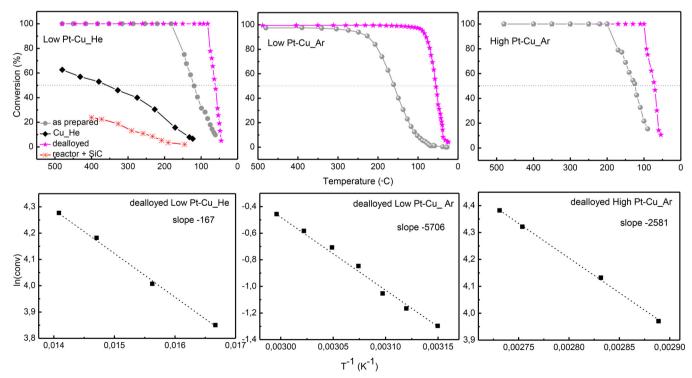


Fig. 7. Conversion vs. temperature curves and Arrhenius plots for the CHC reaction catalysed by the as-prepared and dealloyed Pt-Cu thin films.

Table 3

Kinetic parameters obtained for the CHC reaction catalyzed by the as-prepared and dealloyed Pt-Cu thin films. Comparative data with catalysts in the literature are included.

Catalyst	state	T <sub>50</sub> (°C)	$E_a (kJ mol^{-1})$	conv. at 70 °C (%)	mass of Pt (mg)	Activity (ml min <sup>-1</sup> )	Activity (L min <sup>-1</sup> g <sub>Pt</sub> <sup>-1</sup> )
Low Pt-Cu_He	as deposited	119	22	15	0.150	0.30	2.0
	dealloyed	50	1	71	0.108	1.42	13.15
Low Pt-Cu_Ar	as deposited	159	51	1	0.380	0.02	0.05
	dealloyed	55	47	80	0.219	1.6	7.3
High Pt-Cu_Ar	as deposited	122	38	-	0.736	_	-
	dealloyed	50	21	50	0.82	1	1.22
0.5% Pt/SiC <sup>a</sup> (particles)	_	38	16	80	0.05	1.6	32
0.27% Pt/SiC <sup>b</sup> (particles)	-	34	36	100	0.135	2	15
1% Pt/Co <sub>3</sub> O <sub>4</sub> -ZrO <sub>2</sub> <sup>c</sup> (Pt-substituted)	-	75	39	50	0.25	0.8	3.2

- <sup>a</sup> As reported in Ref. [7].
- <sup>b</sup> As reported in Ref. [8].
- <sup>c</sup> As reported in Ref. [5].

counterparts can be ascribed to the obtention of Pt-enriched, more amorphous and disperse samples. The relative increase in the activity with respect to the as-prepared samples (measured as a decrease in the  $T_{50}$ , the temperature at which 50% conversion is achieved) is higher for the dealloyed Low Pt-Cu\_Ar sample than for the others, which can be attributed to the higher efficiency in the dealloying process.

For a comparison between dealloyed samples, the activity (in  $L_{H2}$ ·min  $^{-1}$   $g_{Pt}$   $^{-1}$ ) was calculated from the curves at 70 °C and the results are shown in Table 3. The activity trend is d-Low Pt-Cu\_He > d-Low Pt-Cu Ar > > d-High Pt-Cu Ar.

Surface composition does not explain the trend, as the amount of Pt<sub>surface</sub> is similar for the three dealloyed samples (Table 2). The Pt oxidation states do not explain the trend either. Our previous studies on Pt particles over different supports showed that under oxidizing conditions, semi-oxidized Pt-surfaces are more active than the completely oxidized ones [7]. Under this hypothesis, d-High Pt-Cu\_Ar should be the most active because of its mostly metallic surface. However, its higher crystallite size might explain its lower activity. The differences in activity between both d-Low Pt-Cu\_He/Ar catalysts cannot be explained in terms of crystal size because in both cases the size is similar (3–4 nm). The open porous structure of d-Low Pt-Cu\_Ar should lead to a higher surface roughening and thus a higher activity, but this does not occur.

Previous studies using synchrotron-based Anomalous X-ray Diffraction (AXRD) and X-ray scattering demonstrated that the formation of a Pt-enriched surface and a Pt-Cu interior leads to a compressive surface lattice strain, which reduces the Pt-O bond strength, increasing the activity towards the ORR [22,23a]. The magnitude of the strain is reduced when the thickness of the Pt-enriched surface increases because the structure relaxes more. Based on these works, we explain the higher activity of d-Low Pt-Cu\_He (Pt<sub>surface</sub> 96%, Pt<sub>bulk</sub> 71%) with respect to d-Low Pt-Cu\_Ar (Pt<sub>surface</sub> 98%, Pt<sub>bulk</sub> 95%). The first sample clearly shows a compositional profile in which the surface is significantly Pt-enriched with respect to the interior, leading to a more strained surface than the latter, which has a more relaxed structure due to its uniform composition [22,2a3]. The correlation between surface lattice strain and activity suggests that for both catalysts under our conditions, breaking the Pt-O bond is the limiting step of the reaction.

The Arrhenius plots were obtained from the linear portion of the conversion-temperature curves and the results are reported in Fig. 7. The apparent activation energies (AAEs) were calculated (Table 3). The dealloyed Low Pt-Cu\_He sample has the lowest AAE of the three (1 kJ mol $^{-1}$ ), followed by the d-High Pt-Cu\_Ar and d-Low Pt-Cu\_Ar samples (21 and 47 kJ mol $^{-1}$ , respectively). The AAE of the d-Low Pt-Cu\_He sample is in the range of the lowest ever reported for this reaction.

It is known that under oxidizing conditions, oxidized surfaces (such as d-Low Pt-Cu\_He/Ar) catalyse the reaction through an Eley-Rideal

mechanism, while for semi-oxidized surfaces (such as d-High Pt-Cu\_Ar) the overall mechanism is a mixture of the Eley-Rideal and the Langmuir-Hinselwood pathways [42]. This explains why the comparison of the three AAES is not straightforward, and only the Low Pt-Cu\_He/Ar samples will be compared. In these samples, weakly adsorbed hydrogen molecules react with chemisorbed oxygen species with no competition for adsorption sites (Eley-Rideal) [42]. The differences in AAEs could be attributed to the distinct lowering of the bonding strength for Pt-O caused by surface strain. Under these conditions, the limiting step must be the desorption of oxygenic species bound to Pt, similar to what occurs in the oxygen reduction reaction (ORR) in fuel cells, and this step is favoured for d-Low Pt-Cu He [43].

The activity of d-Low Pt-Cu\_He  $(13.15\,L_{H2}\,min^{-1}\,g_{Pt}^{-1})$  was compared to other catalysts form our previous works and tested under identical conditions. As shown in Table 4, the activity is similar to the one obtained for  $(11~\pm~4)$  nm Pt nanoparticles  $(15\,L_{H2}\,min^{-1}\,g_{Pt}^{-1})$  and lower than that obtained for  $(5~\pm~4)$  nm Pt nanoparticles  $(32\,L_{H2}\,min^{-1}\,g_{Pt}^{-1})$  on SiC supports [7,8]. Compared to other supports, the activity of d-Low Pt-Cu\_He is higher than that of Pt/Co<sub>3</sub>O<sub>4</sub>-ZrO<sub>2</sub> composite  $(1\%~Pt\text{-doped};~3.2\,L_{H2}\,min^{-1}\,g_{Pt}^{-1})$  but in this case the comparison is not straightforward since the latter catalyst was tested in stoichiometric  $H_2/O_2$  ratio, and the reaction rate is intrinsically lower in these conditions [5]. These results show that the activities of the dealloyed supported catalytic coatings are competitive with respect to powdery Pt-impregnated and Pt-doped catalysts reported in the literature.

As stated above, experiments were conducted using a single SiC monolithic piece coated with 300 nm thin film catalysts. This film thickness was optimized to obtain a full conversion vs. temperature curve for a proper comparison of the catalysts under nearly isothermal conditions. Under these conditions, the room temperature activity of the dealloyed samples is negligible. To evaluate the RT (23 °C) conversion of the d-Low Pt-Cu\_He/Ar catalysts, experiments were conducted by increasing the number of SiC-supported thin-film monolithic catalysts. For both samples, measurable conversion was achieved when loading the reactor with three monolithic catalysts with a consequent increase in temperature. The results are shown in Table S.1. (in SI). The highest conversion and increase in temperature ( + 5 °C) were achieved by the d-Low Pt-Cu\_He catalyst (1.85  $L_{\rm H2}\,{\rm min}^{-1}\,{\rm g_{Pt}}^{-1}$ ) followed by d-Low Pt-Cu\_Ar (0.28  $L_{\rm H2}\,{\rm min}^{-1}\,{\rm g_{Pt}}^{-1}$ , + 0.6 °C temperature increase), in accordance with the activity trend discussed above.

In terms of a commercial application, durability is very important. For this reason, we tested the durability of the d-Low Pt-Cu\_He catalyst in cycles. The results in Figure S.3. (as Supporting information) show a certain activation upon cycling, demonstrating that the catalyst is durable, as expected for a Pt catalyst under oxidizing conditions [6–8].

#### 4. Conclusions

In this paper, we prepared Pt-Cu thin films of controlled microstructure and composition by magnetron sputtering to be used for the first time as catalysts for the combustion of hydrogen under oxidizing conditions. The samples were studied before and after dealloying to obtain more efficient nanoporous Pt-based catalysts. The fabrication of these catalytic films is presented as an alternative to the widely investigated supported nanoparticles. The sputtering deposition of the films was performed using low-cost versatile Pt-Cu targets (pure Cu target with Pt strips), which allowed the selection of the catalyst composition by varying the number of Pt strips and the process gas.

The use of Ar or He as the deposition gases allowed the microstructure of the films to be changed significantly at a constant Pt-composition. Thanks to this, it was possible to evaluate the effect of the microstructure on the activity before and after the dealloying process.

Dealloying permitted us to increase the activity of the samples to reach near room- temperature conversion. The fabrication of closed-porous Pt-Cu samples using He as the sputtering gas permitted to obtain the highest activity upon dealloying. The closed-porous structure is a kinetic barrier for complete Cu dissolution, yielding a compositional profile in which the surface is significantly Pt-enriched with respect to the interior. This vertical inhomogeneity leads to a more strained surface than that of the Ar-deposited, open porous sample, which has a more relaxed structure due to its uniform composition after dealloying. The catalytic activity of these two samples was interpreted in terms of the Eley-Rideal mechanism, in which desorption of oxygenic species bound to Pt is the limiting step.

The use of magnetron-sputtered Pt-Cu precursors with low Pt content is thus proposed as a strategy to generate nanoporous Pt-based catalysts upon dealloying with high conversion and durability at nearly RT conditions to eliminate the undesired  $\rm H_2$  in the exhaust gas of a fuel cell.

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#### Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:https://doi.org/10.1016/j.apcatb.2018.04.064.

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